

Comparison Between the Noise Performance of Double- and Single-Gate InP-Based HEMTs

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Abstract—The noise performance of InAlAs/InGaAs double-gate (DG) and standard high-electron-mobility transistors (HEMTs) is analyzed by means of an ensemble 2-D Monte Carlo simulator. The DG-HEMT is found to have a better noise behavior than the single-gate (SG) device. The results show a moderate decrease of the P and R noise parameters for the DG HEMT with respect to that of the SG device, since current fluctuations due to electrons injected into the buffer are eliminated. Moreover, the DG HEMT reveals a significantly lower extrinsic minimum noise figure NF_{\min} and a higher associated gain G_{ass} , not only due to the better intrinsic performance but also to the lower contact resistances.

Index Terms—Double-gate high-electron-mobility transistor (DG-HEMT), Monte Carlo (MC) simulations, noise behavior.

I. INTRODUCTION

TO FURTHER improve the high-frequency low-noise behavior of InAlAs/InGaAs high-electron-mobility transistors (HEMTs), double-gate (DG) devices have been recently developed [1]–[3]. The DG geometry (a gate is placed on each side of the conducting channel) offers numerous advantages over conventional single-gate (SG) devices, such as counteracting the effect of carrier injection into the buffer, since no buffer is used in the structure, and providing a better charge control. Thus, the DG device exhibits a better pinch-off behavior, lower output conductance g_d , and a higher transconductance g_m . Moreover, the lower resistance of the gate contact R_g leads to a considerably improved extrinsic dynamic behavior (in terms of f_{max}). The source and drain parasitic resistances, R_s and R_d , respectively, are also lower due to the higher electron concentration. Due to all these advances introduced by the DG architecture, an improvement of the intrinsic and extrinsic noise performance is also expected. To clarify this point, in this brief, we perform a full theoretical study of the noise

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behavior of an $\text{In}_{0.52}\text{Al}_{0.48}\text{As}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ 100-nm-gate DG HEMT by comparing it with the corresponding standard SG structure. We make use of a semiclassical 2-D ensemble Monte Carlo (MC) simulator [4], [5], which can reproduce the static and dynamic behavior of the fabricated DG transistors [6] and has proved to be a very helpful tool in the analysis of noise behavior in devices in which an accurate description of the microscopic dynamics of carriers is essential. The intrinsic noise performance is studied in terms of the P , R , and C parameters [7] and the extrinsic one in terms of the minimum noise figure NF_{\min} , the noise resistance R_n , and the associated gain G_{ass} [8].

This brief is organized as follows. In Section II, the MC model employed in the analysis is described. Next, the main results of this brief are presented in Section III. Finally, in Section IV, the most important conclusions are drawn.

II. MC MODEL

For the calculations, we make use of a semiclassical ensemble MC simulator self-consistently coupled with a 2-D Poisson solver, whose validity has been checked for conventional SG [4], [5] and DG HEMTs [6]. The devices under analysis are a recessed 100-nm gate $\text{In}_{0.52}\text{Al}_{0.48}\text{As}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ DG HEMT and the corresponding standard SG HEMT. The detailed topology is shown in Fig. 1. The width of the devices W is 100 μm , and the layer structure is similar to that of the fabricated transistors. The SG HEMT consists of an InP substrate (not simulated), a 200-nm $\text{In}_{0.52}\text{Al}_{0.48}\text{As}$ buffer followed by a 20-nm-thick $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ channel, three layers of $\text{In}_{0.52}\text{Al}_{0.48}\text{As}$ (a 5-nm spacer, a $5 \times 10^{12}\text{-cm}^{-2}$ δ -doped layer modeled as a 5-nm layer doped at 10^{19} cm^{-3} , and a 12-nm Schottky layer), and, finally, a 10-nm-thick $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ cap layer (doped $6 \times 10^{18}\text{ cm}^{-3}$). In the DG HEMT, the buffer is suppressed and substituted by a layer structure symmetrical to that at the top of the channel.

Previously to the noise characterization of the devices, the dynamic performance must be determined. The procedure [4]–[6], [9] is the same for both types of devices, which is correct as long as the DG HEMT works in common mode, i.e., being identical the potential applied at both gate electrodes ($V_{\text{GS1}} = V_{\text{GS2}} = V_{\text{GS}}$). Once calculated the Y parameters, the intrinsic P , R , and C noise parameters [7] are evaluated. They represent the drain and the gate current noise and their cross correlation, respectively. Then, the extrinsic minimum noise figure NF_{\min} [8], which indicates the noise added by the device to the signal that is amplifying, and

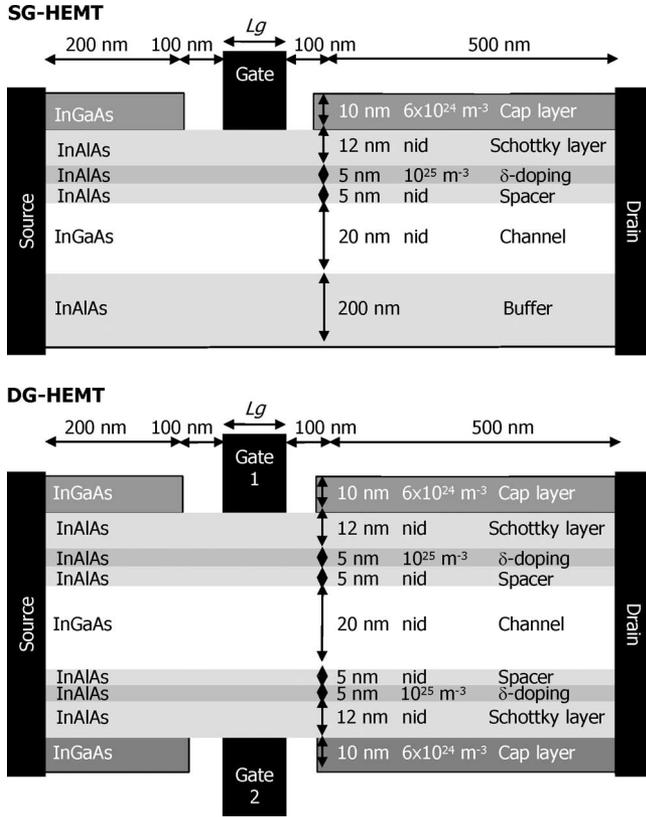


Fig. 1. Schematic drawing of the simulated SG and DG HEMTs. $L_g = 100$ nm.

the associated gain G_{ass} are evaluated by taking into account both intrinsic and extrinsic noise sources. Another important parameter to be calculated (having a key influence for circuit design) is the noise resistance R_n , which is a measure of the sensibility of NF_{min} to the changes of the input admittance with respect to its optimum value [8].

III. RESULTS

To better understand their noise performances, we have previously analyzed the static and dynamic behavior of both SG and DG HEMTs [6]. The insets of Fig. 2 show the comparison between the experimental and MC extrinsic output characteristics of both devices. The drain-current I_D provided by the DG HEMT is about twice that given by the SG transistor, since the electron concentration in the DG-HEMT channel is significantly higher due to the presence of two charge-accumulation regions. Regarding the dynamic behavior, we show the extrinsic cutoff frequencies f_{max} and f_t as main parameters. The MC values of f_{max} and f_t as a function of the drain-current are shown in Fig. 2 for both 100-nm-gate SG [Fig. 2(a)] and DG [Fig. 2(b)] HEMTs with 100- μm gate width. The values taken by f_{max} are higher in the DG HEMT than in the SG structure. Particularly, the maximum values of f_{max} are 286 GHz for the DG HEMT and 226 GHz for the SG HEMT, in good agreement with the results of the measurements 288 and 220 GHz, respectively [2]. The simulations and the experiments show similar values for f_t for both devices, around 200 GHz

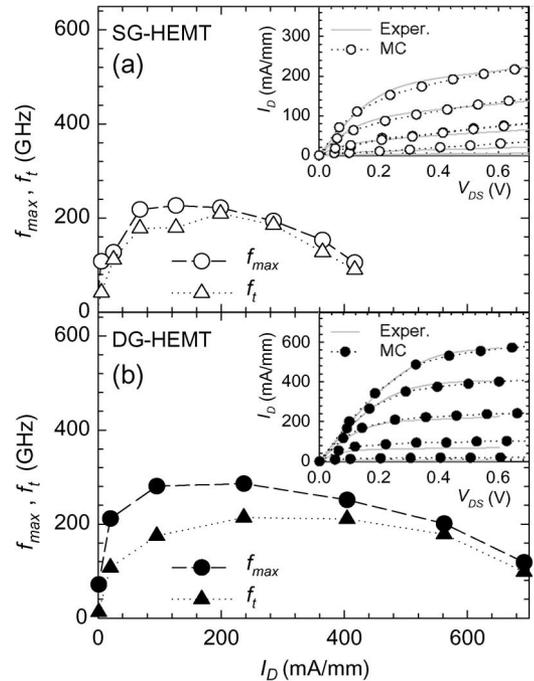


Fig. 2. MC values of f_{max} and f_t versus I_D for the (a) SG and (b) DG HEMTs. $V_{\text{DS}} = 0.5$ V. Inset: Experimental and MC extrinsic output characteristics, where the gate voltage of the top curves is $V_{\text{GS}} = 0.0$ V and the step of the gate bias is $\Delta V_{\text{GS}} = 0.1$ V for both sets of curves.

(the intrinsic cutoff frequency f_c is also similar, since the increase of g_m in the DG HEMT is compensated by its higher gate capacitances). The improvement of f_{max} in the DG device is higher than that of f_t , due to the reduced values of R_g and g_d , which have a significant influence on f_{max} without much affecting the value of f_t . These results have already been widely explained in [6].

Concerning the intrinsic noise behavior, in Fig. 3, the intrinsic P [Fig. 3(a)], R [Fig. 3(b)], and C [Fig. 3(c)] noise parameters are shown as a function of I_D for the simulated DG and SG HEMTs, where $V_{\text{DS}} = 0.5$ V. For a better understanding of the figure, since the MC results for R and C are not very accurate due to the uncertainty in the calculation of the gate noise [5] (and also the value of P for very low I_D , when g_m is practically zero), their respective tendency lines have been drawn. Moreover, it must be pointed out that the gate leakage current and its consequent shot noise, that may affect the value of R (mainly near pinch-off), are not included in our model. P and R , representing, respectively, the noise due to the drain and gate current fluctuations, take lower values in the DG HEMT than in the SG device. This happens because carriers in the DG device are completely confined in the channel, and the current fluctuations due to electrons injected into the buffer are avoided. The change between low/high horizontal velocity of electrons in the buffer/channel leads to drain-current fluctuations, while the associated vertical motion generates an excess of gate current noise. Thus, the suppression of these real space-transfer processes reduces both drain and gate current noise. On the other hand, C is about the same for both types of devices, since the electron dynamics inside the channel and the gate-channel coupling are similar.

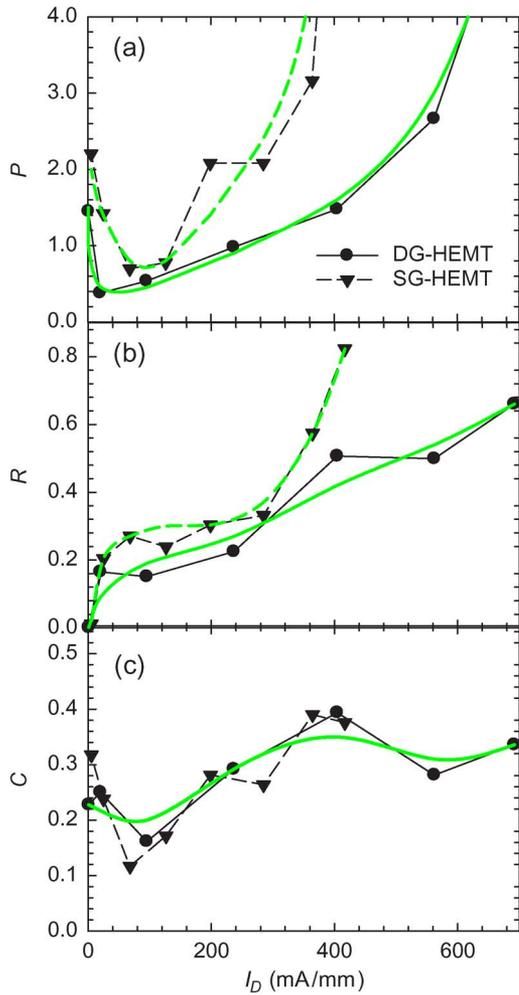


Fig. 3. MC values of (a) P , (b) R , and (c) C parameters versus I_D for the 100-nm-gate DG and SG HEMTs. $V_{DS} = 0.5$ V. Their corresponding tendency lines are also plotted.

The extrinsic noise performance of the devices is described through the parameters NF_{min} and R_n , together with G_{ass} . In Fig. 4, we show their MC values at 94 GHz for $V_{DS} = 0.5$ V as a function of I_D for both DG and SG HEMTs. The corresponding intrinsic values, calculated without considering the parasitic contact resistances R_s , R_d , and R_g , are also plotted for comparison. The minimum noise figure shows the typical U-shape, mainly due to the influence of R_n , which increases at both high (due to the increase of the drain noise, associated with the P parameter) and low (due to the decrease of the cutoff frequency) drain-current. The intrinsic NF_{min} is lower in the DG than in the SG HEMT (the minimum values are 1.1 and 1.4 dB, respectively) due to the reduction of the intrinsic drain and gate noise (lower P and R). When the contact resistances are taken into account, the minimum values taken by NF_{min} are 2.1 dB (for $I_D = 21$ mA/mm) for the DG HEMT and 2.9 dB (for $I_D = 68$ mA/mm) for the SG device. Therefore, the extrinsic NF_{min} is significantly improved by the use of the DG architecture, due to the better intrinsic behavior and the lower parasitic contact resistances. The extrinsic R_n and G_{ass} are also much improved in the DG structure, thus allowing both for a better noise matching and

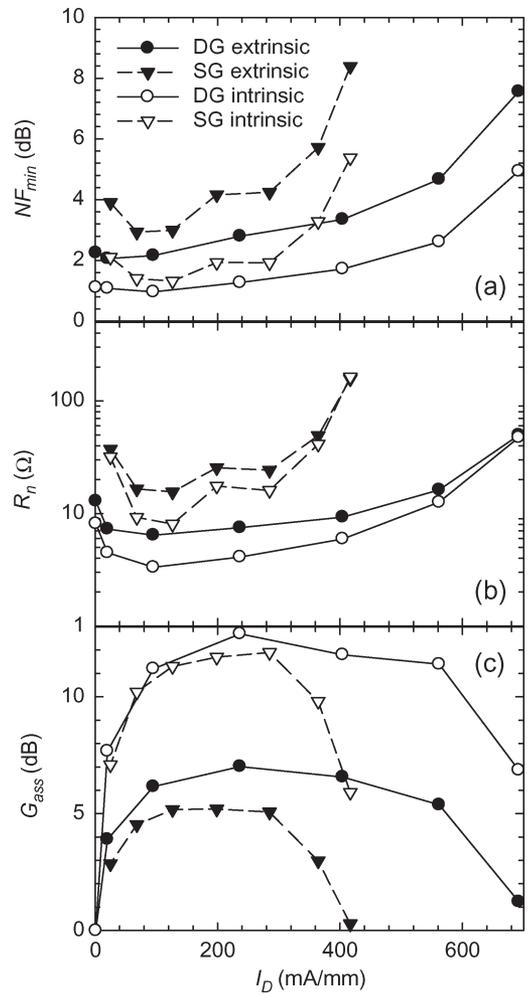


Fig. 4. Intrinsic and extrinsic MC values of the (a) NF_{min} , (b) R_n , and (c) G_{ass} versus I_D for the 100-nm-gate DG and SG HEMTs at 94 GHz. $V_{DS} = 0.5$ V.

a higher gain at low-noise conditions and, as a consequence, a more flexible monolithic microwave integrated-circuit design.

Fig. 5 shows the frequency dependence of NF_{min} and G_{ass} for both HEMTs at the I_D providing the minimum of NF_{min} . At these particular values of I_D , the best values of NF_{min} involve similar values of G_{ass} for both devices. The intrinsic values and those obtained considering only R_s and R_d (and not R_g) in the calculations are shown in Fig. 5. In all cases, the well-known increase of NF_{min} and decrease of G_{ass} with frequency is clearly observed. Moreover, in both types of devices, for this particular value of gate width $W = 100$ μ m, the increase of NF_{min} due to R_s and R_d is larger as compared to that coming from the presence of R_g . However, the contribution of the different contact resistances to the extrinsic value of NF_{min} depends on the value of W , since R_g is proportional to W , while R_s and R_d are proportional to $1/W$. In Fig. 6, we show the values of NF_{min} [Fig. 6(a)], R_n [Fig. 6(b)], and G_{ass} [Fig. 6(a)] as a function of W at 94 GHz for both simulated DG and SG devices. For these calculations, we have supposed that the extrinsic capacitances are proportional to W , which is a good approximation only for large W .

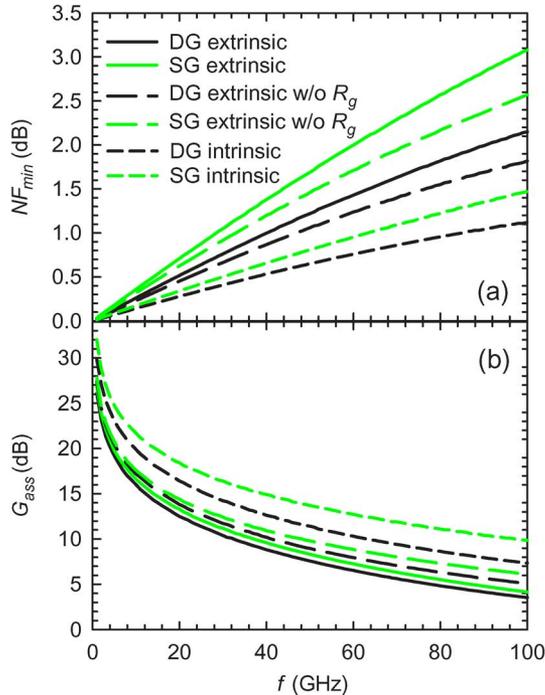


Fig. 5. Intrinsic and extrinsic MC values of (a) NF_{\min} and (b) G_{ass} versus frequency for the 100-nm-gate DG and SG HEMTs with $W = 100 \mu\text{m}$ for the bias point providing the minimum of NF_{\min} (at $V_{\text{DS}} = 0.5 \text{ V}$). In addition, the values calculated only considering R_s and R_d (and not R_g , labeled as extrinsic without R_g) are plotted for comparison.

Indeed, for very short W , the capacitances reach a certain saturation value, which leads to a deterioration of NF_{\min} and G_{ass} [5], [10]. Nevertheless, these offset capacitances do not alter the comparison between the behavior of the SG and the DG HEMT, since this effect equally affects both devices. Notably, the difference between the intrinsic values of NF_{\min} at 94 GHz for the DG and the SG devices, 0.3 dB, is increased to 0.7 dB when R_s and R_d are considered in the calculations (since their values in the DG HEMT are lower). In both cases, the values of NF_{\min} are independent of W , as expected from the identical proportionality to $1/W$ of the contributions to the total noise of the intrinsic device and the R_s and R_d parasitic resistances. On the other hand, when all the contact resistances are taken into account, the values of NF_{\min} increase when increasing W (with a decrease of G_{ass}), since R_g is proportional to W . Moreover, as a result of the lower R_g of the DG HEMT, the difference of NF_{\min} with respect to the SG device increases with W , where, for example, 0.75 dB for $W = 50 \mu\text{m}$, 0.9 dB for $W = 100 \mu\text{m}$, and 1.4 dB for $200 \mu\text{m}$ (0.7 dB is coming from the difference in the intrinsic noise and the values of R_s and R_d). As a consequence, since small values of W are used for high-frequency low-noise applications, the smaller values of R_s and R_d of the DG with respect to the SG devices are much more important than those of R_g for the achievement of better noise performances. The same dependences are observed for G_{ass} [Fig. 6(c)] but taking similar extrinsic values for both devices. Finally, the intrinsic and extrinsic values of R_n [Fig. 6(b)] increase when decreasing W , but less significantly in the DG HEMT, thus providing an easier noise matching for lower W ,

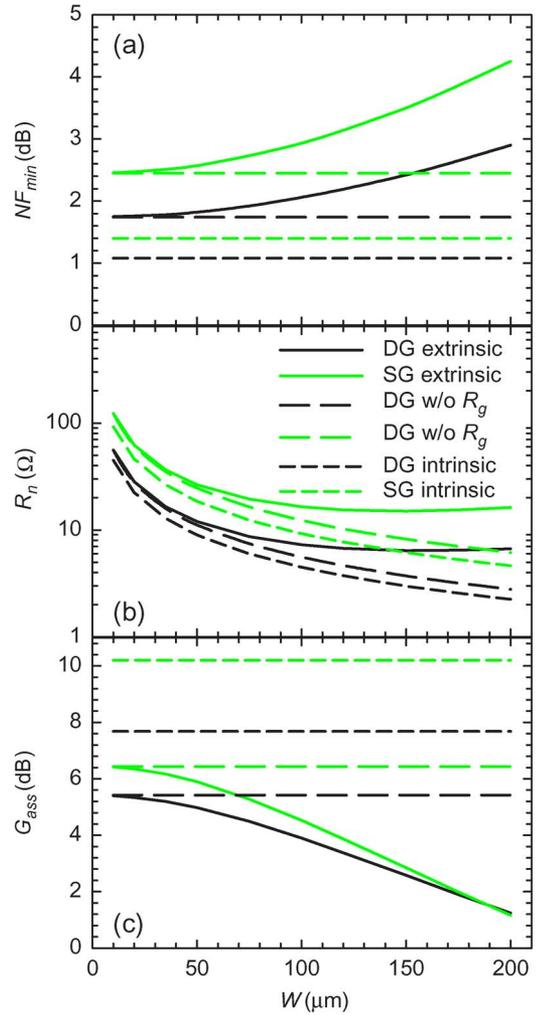


Fig. 6. Intrinsic and extrinsic MC values of (a) NF_{\min} , (b) R_n , and (c) G_{ass} versus gate width W for the 100-nm-gate DG and SG HEMTs at 94 GHz for the bias point providing the minimum of NF_{\min} (at $V_{\text{DS}} = 0.5 \text{ V}$). In addition, the values calculated only considering R_s and R_d (and not R_g , labeled as extrinsic without R_g) are plotted for comparison.

which eases the circuit design for high-frequency low-noise applications.

IV. CONCLUSION

We have presented an MC-based study of DG HEMTs comparing the noise performance with standard SG devices. The results of our simulations show that the intrinsic P and R noise parameters in the DG are lower than in SG HEMT due to the suppression of the current fluctuations originated by the injection of electrons into the buffer. Furthermore, the extrinsic noise behavior (in terms of NF_{\min} , G_{ass} , and R_n) is significantly improved due not only to the better intrinsic noise performance but also to the lower R_s , R_d , and R_g (the latter being increasingly important for larger W).

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